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## Bescheinigung

### Certificate

Die angehefteten Unterlagen stimmen mit der ursprünglich eingereichten Fassung der auf dem nächsten Blatt be-zelchneten internationalen Patentanmeldung überein.

The attached documents are exact copies of the international patent application described on the following page, as originally filed.

Attestation

Les documents fixés à cette attestation sont conformes à la version initialement déposée de la demande de brevet interdéposée de la demande de brevet international spécifiée à la page suivante.

Den Haag, den The Hague, La Haye, le

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Der Präsident des Europäischen Patentamts Im Auftrag For the President of the European Patent Office Le Président de l'Office européen des brevets

SUBMITTED OR TRANSMITTED IN COMPLIANCE WITH RULE 17.1(a) OR (b) Patentanmeldung Nr. PCT/EP 03/00482 Patent application no. Demande de brevet n°

Blatt 2 der Bescheinigung Sheet 2 of the certificate Page 2 de l'attestation



Anmeldung Nr.: Application no.:

Demande nº:

PCT/EP 03/00482

Anmelder: Applicant(s):

Demandeur(s):

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Bezeichnung der Erfindung: 3. SCELZA, Cristiana - Milano, Italy (US only)

Title of the invention: Titre de l'invention:

Cable with recyclable covering layer

Anmeldetag: Date of filing:

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The applicant's name at the time of filing of the application was as follows: PIRELLI.S.p.A

The registration of the change has taken affect on 27 November 2003 (27.11.2003)

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#### CABLE WITH RECYCLABLE COVERING LAYER

The present invention relates to a cable with In particular, layer. recyclable covering invention relates to a cable for transporting or distributing medium or high voltage electric energy, wherein an extruded covering layer based on a thermoplastic polymer material in admixture with a good mechanical with dielectric liquid enabling, present, electrical properties is particular, the use of high operating temperatures and the transportation of high power energy.

Said cable may be used for both direct current (DC) or alternating current (AC) transmission or distribution.

οf products requirement for The environmental compatibility, composed of materials which, in addition to not being harmful to the environment during production or utilization, may be easily recycled at the end of their life, is now fully accepted in the field of electrical telecommunications cables.

However the use of materials compatible with the environment is conditioned by the need to limit costs while, for the more common uses, providing a better than that orperformance equal to conventional materials.

In the case of cables for transporting medium and high voltage energy, the various coverings surrounding the conductor commonly consist polyolefin-based crosslinked polymer, in particular crosslinked polyethylene (XLPE), or elastomeric ethylene/propylene (EPR) or ethylene/propylene/diene crosslinked. copolymers, also (EPDM) crosslinking, effected after the step of extrusion of the polymeric material onto the conductor, gives

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the material satisfactory mechanical and electrical properties even under high temperatures both during continuous use and with current overload.

is well known however that crosslinked materials cannot be recycled, so that manufacturing wastes and the covering material of cables which have reached the end of their life may be disposed of only by incineration. . .

Electric cables are also known having their insulation consisting of a multi-layer wrapping of a paper or paper/polypropylene laminate impregnated with a large quantity of a dielectric liquid (commonly known as mass impregnated cables or also oil-filled cables). By completely filling the spaces present in the multi-layer wrapping, the dielectric liquid prevents partial discharges arising with consequent break down of the electrical insulation. As dielectric liquids products are commonly used such as mineral oils, polybutenes, alkylbenzenes and 4,543,207, US like (see, for example, us 4,621,302, EP 987,718, WO 98/32137).

It is however well known that mass impregnated compared with drawbacks numerous cables have extruded insulation cables, so that their use is fields to specific currently restricted 25 application, in particular to the construction of and very high voltage direct transmission lines, both for terrestrial and particular for underwater installations. In this respect, the production of mass impregnated cables 30 is particularly complex and costly, both for the high cost of the laminates and for the difficulties during the steps of wrapping encountered laminate and then of impregnating it with the dielectric liquid. In particular, the dielectric 35 liquid used must have low viscosity under

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temperatures to allow rapid and uniform impregnation, while at the same time it must have a low tendency to migrate during installation and operation of the cable to prevent liquid loss from the cable ends or from accidentally breaks on the cable. In addition, mass impregnated cables cannot be recycled and their use is limited to an operating temperature of less than 90°C.

Within non-crosslinked polymeric materials, it is known to use high density polyethylene (HDPE) for covering high voltage cables. HDPE has however the drawback of a lower temperature resistance than KLPE, both to current overload and during operation.

Thermoplastic low density polyethylene (LDPE) insulating coverings are also used in medium and high voltage cables: again in this case, these coverings are limited by a too low operating temperature (about 70°C).

International Patent Application WO 99/13477 discloses an insulating material consisting of a 20 thermoplastic polymer forming a continuous phase incorporates a liquid or easily meltable dielectric forming a mobile interpenetrating phase within the solid polymer structure. The weight ratio of thermoplastic polymer to dielectric is between 25 95:5 and 25:75. The insulating material may produced by mixing the two components while hot either batchwise or continuously (for example, by means of an extruder). The resultant mixture is then granulated and used as insulating material 30 producing a high voltage electric cable by extrusion onto a conductor. The material may be used either in thermoplastic or crosslinked form. As thermoplastic polymers are indicated: polyolefins, polyacetates, polyketones, polyesters, polymers, cellulose 35 polyacrylates, polyamides and polyamines. The use of

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low crystallinity is particularly polymers of suggested. The dielectric is preferably a synthetic mineral oil of low or high viscosity, particular a polyisobutene, naphthene, polyaromatic, α-olefin or silicone oil.

International Patent Application WO 02/03398 in the name of the Applicant, discloses a cable comprising at least one electrical conductor and at extruded covering layer based one thermoplastic polymer material in admixture with a wherein said thermoplastic liquid, dielectric material comprises a propylene homopolymer or a copolymer of propylene with at least one olefin comonomer selected from ethylene and an  $\alpha$ -olefin other than propylene, said homopolymer or copolymer having a melting point greater than or equal to 140°C and a melting enthalpy of from 30 J/g to 100 J/g. Said dielectric liquid comprises at least one alkylaryl hydrocarbon having at least two noncondensed aromatic rings and a ratio of number of 20 aryl carbon atoms to total number of carbon atoms greater than or equal to 0.6, preferably greater than or equal to 0.7.

International Patent Application WO 02/27731 in the name of the Applicant, discloses a cable 25 comprising at least one electrical conductor and at layer based on one extruded covering thermoplastic polymer material in admixture with a said thermoplastic wherein liquid, dielectric material comprises a propylene homopolymer or 30 copolymer of propylene with at least one olefin componer selected from ethylene and an  $\alpha$ -olefin other than propylene, said homopolymer or copolymer having a melting point greater than or equal to 140°C and a melting enthalpy of from 30 J/g to 100 35 J/g. Said dielectric liquid comprises at least one . 5

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diphenyl ether, non-substituted or substituted with at least one linear or branched, aliphatic, aromatic or mixed aliphatic and aromatic  $C_1$ - $C_{30}$  hydrocarbon radical.

However, the prior art above cited presents some drawbacks.

As a matter of fact, Applicant noticed that the of a dielectric liquid to a polymer significant determine a should both material electrical properties (in in its increase strength), dielectric particular, its impairing its thermomechanical characteristics and without resulting in exudation of the dielectric liquid from the polymer material. In particular, the resultant cable should give substantially constant mechanical and electrical performances with time and hence high reliability, even at high operating and beyond, 90°C least temperatures (at particular at operating temperature up to 110°C for continuous use and up to 140°C in the case of current overload). In particular, Applicant noticed that the presence of two phases, e.g. a continuous phase of a thermoplastic material and an additional phase incorporated therein of a dielectric liquid, with the consequent microscopically non homogeneous dispersion of said dielectric liquid onto said thermoplastic material, does not allow to obtain all the above reported characteristics.

The Applicant has now found that it possible to overcome said drawbacks by using, as recyclable polymer base material, at least one thermoplastic propylene homopolymer or copolymer or a mechanical mixture of said at least one thermoplastic propylene homopolymer or copolymer with at least one elastomeric copolymer of ethylene with at least one aliphatic α-olefin, and optionally a polyene, mixed

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with at least one dielectric liquid as hereinafter possesses composition resultant defined. The thermomechanical suitable flexibility, excellent and high electrical performance, characteristics such as to make it particularly suitable for forming 5 at least one covering layer, and in particular an electrical insulating layer, of a medium or high voltage cable of high operating temperature, of at least 90°C and beyond, in particular at operating temperature up to 110°C for continuous use and up to 10 current overload. the case ο£ in liquid suitable for implementing the dielectric invention has high compatibility with the polymer base material and high efficiency in the sense of consequently performance, electrical improving 15 allowing the use of small quantities (e.g quantities not higher than the saturation concentration of the dielectric liquid in the polymer base material) of said dielectric liquid such as not to impair the thermomechanical characteristics of the insulating 20 layer and to avoid the exudation of said dielectric liquid from the polymer base material.

High compatibility between the dielectric liquid and the polymer base material allows to obtain a dispersion homogeneous of microscopically dielectric liquid in the polymer base material. Moreover, the dielectric liquid suitable for forming the cable covering layer of the present invention comprises a small quantity of polar compounds, order to avoid a significant increasing of the dielectric losses. It has to be noticed also that the use of a dielectric liquid with a relatively low melting point (e.g, a melting point not higher than 80°C) does not give rise to manufacturing problems both during the mixing with the polymer material and during the production of the cable. As a matter of

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fact, the low melting point allows to an easier handling of the dielectric liquid which may be easily melted without the need of additional and complex manufacturing steps (e.g., a melting step of the dielectric liquid) and/or apparatuses. Moreover, Applicant noticed also that, when dielectric liquid is aromatic, high compatibility with the polymer base material may be achieved even in the presence of dielectric liquid with a low ratio of number of aromatic carbon atoms to total number of carbon atoms (e.g., ratio lower than 0.6).

The Applicant has also noticed that the addition of said dielectric liquid reduces or even eliminates the optical phenomena commonly known as "stress whitening" thanks to the fact that said dielectric liquid is microscopically homogeneously dispersed in the polymer material.

aspect, the present first a According to invention relates to a cable comprising at least one least one extruded electrical conductor and at covering layer based on a thermoplastic polymer material in admixture with a dielectric liquid, wherein:

said thermoplastic polymer material is selected from:

- (a) at least one propylene homopolymer or at least one copolymer of propylene with at least one olefin comonomer selected from α-olefin other an and ethylene said homopolymer or propyleme, having a melting point greater than or equal to 130°C and a melting enthalpy of from 20 J/g to 100 J/g;
- (b) a mechanical mixture comprising at least one propylene homopolymer or copolymer (a) and (c) at least one elastomeric copolymer of

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ethylene with at least one aliphatic  $\alpha$ olefin, and optionally a polyene;

- the concentration by weight of said dielectric liquid in said thermoplastic polymer material is less or equal to the saturation concentration of said dielectric liquid in said thermoplastic polymer material;
- following the has said dielectric liquid characteristics:
- an amount of polar compounds lower than or 10 equal to 2.5% by weight with respect to the total weight of the dielectric liquid;
  - a melting point or a pour point lower than 80°C;
- a ratio of number of aromatic carbon atoms 15 with respect to the total number of carbon atoms lower than 0.6, when the dielectric liquid is aromatic.

In the present description and in the subsequent claims, the term "conductor" means a conducting 20 element as such, of elongated shape and preferably of a metallic material, or a conducting element coated with a semiconducting layer.

The saturation concentration of the dielectric liquid in the thermoplastic polymer material may be determined by a liquid absorption method on Dumbell samples: further details regarding said method will be described in the examples given hereinbelow.

The amount of polar compounds of the dielectric liquid may be determined according to ASTM standard 0 E D2007-02.

The melting point may be determined by known techniques such as, for example, by Differential Scanning Calorimetry (DSC) analysis.

The pour point may be determined according to 35 ASTM standard D97.

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The ratio of number of aromatic carbon atoms with respect to the total number of carbon atoms may be determined according to ASTM standard D3238.

According to a first embodiment, the extruded covering layer based on said thermoplastic polymer material in admixture with said dielectric liquid is an electrically insulating layer.

According to a further embodiment, the extruded covering layer based on said thermoplastic polymer material in admixture with said dielectric liquid is a semiconductive layer.

embodiment, According to one preferred propylene homopolymer or copolymer (a) which may be used in the present invention has a melting point of from 140°C to 170°C.

homopolymer propylene Preferably, the copolymer (a) has a melting epthalpy of from 30 J/g to 85 J/g.

Said melting enthalpy  $(\Delta H_m)$  may be determined by Differential Scanning Calorimetry (DSC) analysis. 20

homopolymer propylene the Preferably, a flexural modulus, measured copolymer (a) has standard D790, room ASTM to ' according temperature, of from 30 MPa to 1400 MPa, and more preferably from 60 MPa to 1000 MPa.

homopolymer propylene the Preferably, copolymer (a) has a melt flow index (MFI), measured at 230°C with a load of 21.5 N according to ASTM standard D1238/L, of from 0.05 dg/min to 10.0 dg/min, more preferably from 0.4 dg/min to 5.0 dg/min.

If a copolymer of propylene with at least one used, this latter olefin comonomer (a) is preferably present in a quarktity of less than or equal to 15 mol\*, and more preferably of less than or equal to 10 molt. The olefin comonomer is, in

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particular, ethylene or an  $\alpha$ -olefin of formula  $CH_2$ =CH-R, where R is a linear or branched  $C_2$ - $C_{10}$  alkyl, selected, for example, from: 1-butene, 1-pentene, 4-methyl-1-pentene, 1-hexene, 1-octene, 1-decene, 1-dodecene, or mixtures thereof. Propylene/ethylene copolymers are particularly preferred.

Preferably, said propylene homopolymer or copolymer (a) is selected from:

- 10 (a<sub>1</sub>) a propylene homopolymer or a copolymer of propylene with at least one olefin comonomer selected from ethylene and an α-olefin other than propylene, having a flexural modulus generally of from 30 MPa to 900 MPa, and preferably of from 50 MPa to 400 MPa;
  - (a<sub>2</sub>) a heterophase copolymer comprising a thermoplastic phase based on propylene and an elastomeric phase based on ethylene copolymerized with an α-olefin, preferably with propylene, in which the elastomeric phase is preferably present in a quantity of at least 45 wt% with respect to the total weight of the heterophase copolymer.

particularly preferred of said class (a<sub>1</sub>) is a propylene homopolymer or a copolymer of propylene with at least one olefin commonomer selected from ethylene and an  $\alpha$ -olefin other than propylene, said homopolymer or copolymer having:

- a melting point of from 140°C to 170°C;
- 30 a melting enthalpy of from 30 J/g to 80 J/g;
  - a fraction soluble in boiling diethyl ether in an amount of less than or equal to 12 wt%, preferably from 1 wt% to 10 wt%, having a melting enthalpy of less than or equal to 4 J/g, preferably less than or equal to 2 J/g;
  - a fraction soluble in boiling n-heptane in an

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amount of from 15 wt% to 50 wt%, preferably from 20 wt% to 50 wt%, having a melting enthalpy of from 10 J/g to 40 J/g, preferably from 15 J/g to 30 J/g; and

- a fraction insoluble in boiling n-heptane in an amount of from 40 wt% to 85 wt%, preferably from 50 wt% to 80 wt%, having a melting enthalpy of greater than or equal to 45 J/g, preferably from 50 J/g to 95 J/g.
- 10 Further details concerning these materials and their use in cables covering are given in International Patent Application WO 01/37289 in the name of the Applicant.

The heterophase copolymets of class (a2) are 15 sequential copplymerization i) obtained by propylene, possibly containing minor quantities of at least one olefin comonomer selected from ethylene and an  $\alpha$ -olefin other than ptopylene; and then of: a mixture of ethylene with an α-olefin, possibly with 20 particular propylene, and minor portions of a diene.

Particularly preferred of said class (a2) is a heterophase copolymer in which the elastomeric phase consists of an elastomeric copolymer of ethylene and propylene comprising from 15 wt% to 50 wt% of ethylene and from 50 wt% to 85 wt% of propylene with respect to the weight of the elastomeric phase. Further details concerning these materials and their use in cables covering are given in International Patent Application WO 00/41187 in the name of the Applicant.

Products of class (a<sub>1</sub>) are available commercially for example under the trademark Rexflex WL 105 of Huntsman Polymer Corporation or Borsoft SA 233 CF of Borealis.

Products of class (a2) are available commercially

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for example under the trademark Hifax CA 10 A, Moplen EP 310 G, or Adflex Q 200 F of Basell.

According to one preferred embodiment; elastomeric copolymer of ethylene (c) has a melting enthalpy of less than 30 J/g. The quantity of said elastomeric copolymer (c) is generally less than 70% by weight, preferably of from 20% by weight to 60% by weight, with respect to the total weight of the thermoplastic base material.

With reference to the elastomeric copolymer of 10 "aliphatic term the (c), ethylene generally means an olefin of formula CH2=CH-R, which R represents a linear or branched alkyl group containing from 1 to 12 carbon atoms. Preferably, the aliphatic  $\alpha$ -olefin is selected from propylene, 15 4-methyl-1-1-pentene, isobutylene, pentene, 1-hexene, 1-octene, 1-dodecene, or mixtures thereof. Propylene, 1-hexene and 1-octene particularly preferred.

With reference to the elastomeric copolymer of ethylene (c), the term "polyene" generally means a conjugated or non-conjugated diene, triene tetraene. When a diene comonomer is present, this comonomer generally contains from 4 to 20 carbon is preferably selected from: conjugated or non-conjugated diolefins such as, for 1,4-hexadiene, 1,3-butadiene, example, octadiene, and the like; monocyclic or polycyclic dienes such as, for example, 1,4-cyclohexadiene, 5-ethylidene-2-norbornene, 5-methylene-2-norbornene, vinylnorbornene, or mixtures thereof. When a triene or tetraene comonomer is present, this comonomer generally contains from 9 to 30 carbon atoms and is tetraenes preferably selected from trienes OT containing a vinyl group in the molecule or a 5norbornen-2-yl group in the molecule. Specific

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examples of triene or tetraene comonomers which may be used in the present invention are: 6,10-dimethyl-1,5,9-undecatriene, 5,9-dimethyl-1,4,8-decatriene, 6,9-dimethyl-1,5,8-decatriene, 6,8,9-trimethyl-1,6,8-decatriene, 6,10,14-trimethyl-1,5,9,13-pentadecatetraene, or mixtures thereof. Preferably, the polyene is a diene.

Particularly preferred elastomeric copolymers of ethylene (c) are:

- 10 (C<sub>1</sub>) copolymers having the following monomer composition: 35 mol%-90 mol% of ethylene; 10 mol%-65 mol% of an aliphatic α-olefin, preferably propylene; 0 mol%-10 mol% of a polyene, preferably a diene, more preferably, 1,4-hexadiene or 5-ethylene-2-norbornene (EPR and EPDM rubbers belong to this class);
  - (c<sub>2</sub>) copolymers having the following monomer composition: 75 mol<sup>2</sup>-97 mol<sup>2</sup>, preferably 90 mol<sup>2</sup>-95 mol<sup>2</sup>, of ethylene; 3 mol<sup>2</sup>-25 mol<sup>2</sup>, preferably 5 mol<sup>2</sup>-10 mol<sup>2</sup>, of an aliphatic α-olefin; 0 mol<sup>2</sup>-5 mol<sup>2</sup>, preferably 0 mol<sup>2</sup>-2 mol<sup>2</sup>, of a polyene, preferably a diene (for example ethylene/1-octene copolymers, such as the products Engage of DuPont-Dow Blastomers).

25 According to a preferred embodiment, the dielectric liquid has an amount of polar compounds of between 0.1 and 2.3.

According to a further preferred embodiment, the dielectric liquid has a melting point or a pour point of between -130°C and +80°C.

According to a further preferred embodiment, the dielectric liquid has a ratio of number of aromatic carbon atoms with respect to the total number of carbon atoms of between 0.01 and 0.4.

According to a further preferred embodiment, the dielectric liquid preferably has a dielectric

constant, at 25°C, of less than or equal to 3.5 and preferably less than 3 (measured in accordance with IEC 247).

According to a further preferred embodiment, the dielectric liquid has a predatermined viscosity in order to prevent fast diffusion of the liquid within the insulating layer and hence its outward migration, as well as to enable the dielectric liquid to be easily fed and mixed into the thermoplastic polymer material. Generally, the dielectric liquid of the invention has a viscosity, at 40°C, of between 10 cst and 800 cSt, preferably between 20 cst and 500 cSt (measured according to ASTM standard D445).

According to one preferred embodiment, 15 dielectric liquid may be selected from: mineral oils such as, for example, naphthenic oils, aromatic oils, paraffinic oils, polyaromatic oils, mineral oils optionally containing at least one from oxygen, nitrogen heteroatom selected 20 sulphur; liquid paraffins; vegetable oils such as, for example, soybean oil, linseed oil, castor oil; oligomeric aromatic polyolefins; paraffinic waxes example, polyethylene waxes, such as, for polypropylene waxes; synthetic oils such as, for example, silicone oils, alkyl benzenes (such as, for dodecylbenzene, di (octylbenzyl) toluene), aliphatic esters (such as, for example, tetraesters of pentaerythritol, esters of sebacic acid, phthalic esters), olefin oligomers (such as, for example, 30 hydrogenated polybutenes optionally polyisobutenes); or mixtures thereof. Paraffinic oils and naphthenic oils are particularly preferred.

The dielectric liquid suitable for implementing the invention has good heat resistance, considerable gas absorption capacity, in particular hydrogen

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partial resistance to high absorption, and discharges, so that dielectric losses are limited high electrical high temperature and gradient. The weight ratio of dielectric liquid to thermoplastic polymer material the ρĒ generally between 1:99 and 25:75, invention is 2:98 and 20:80, .and preferably between preferably between 3:97 and 10:90.

According to one preferred embodiment, the cable of the invention has at least one extruded covering layer with electrical insulation properties formed from the thermoplastic polymer material in admixture with the aforedescribed dielectric liquid.

According to a further preferred embodiment, the cable of the invention has at least one extruded covering layer with semiconductive properties formed from the thermoplastic polymer material in admixture with the aforedescribed dielectric liquid. To form a conductive filler layer, a semiconductive generally added to the polymer material. To ensure good dispersion of the conductive filler within the latter polymer material, the thermoplastic preferably selected from propylene homopolymers or copolymers comprising at least 40 wt% of amorphous phase, with respect to the total polymer weight.

According to a further aspect, the present invention relates to a polymer composition comprising a thermoplastic polymer material in admixture with a dielectric liquid, wherein:

- 30 said thermoplastic polymer material is selected from:
  - (a) at least one propylene homopolymer or at least one copolymer of propylene with at least one olefin comonomer selected from ethylene and an α-olefin other than propylene, said homopolymer or copolymer

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having a melting point greater than or equal to 130°C and a melting enthalpy of from 20 J/g to 100 J/g;

- (b) a mechanical mixture comprising at least one propylene homopolymer or copolymer (a) and at least one elastomeric copolymer of ethylene with at least one aliphatic  $\alpha$ olefin, and optionally a polyene;
- the concentration by weight of said dielectric liquid in said thermoplastic polymer material is 10 less or equal to the saturation concentration of said dielectric liquid in said thermoplastic polymer material;
- following dielectric liquid has the said characteristics: 15
  - an amount of polar compounds lower than or equal to 2.5% by weight with respect to the total weight of the dielectric liquid;
  - a melting point or a pour point lower than BO°C;
  - a ratio of number of aromatic carbon atoms with respect to the total number of carbon atoms lower than 0:6, when the dielectric liquid is aromatic.

the present According to a further aspect, 25 polymer use φf the to invention relates hereinabove, the described composition, as polymer base material for preparing a cable covering layer with electrical insulation properties, or for preparing a cable covering layer with semiconductive .30 properties.

In forming a covering layer for the cable of the invention, other conventional components may be added to the aforedefined polymer composition, such water processing aids, antioxidants, retardants, or mixtures thereof.

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Conventional antioxidants suitable for the purpose are for example distearyl- or dilauryl-thiopropionate and pentaerythrityl-tetrakis [3-(3,5-di-t-butyl-4-hydroxyphenyl)propionate], or mixtures thereof.

Processing aids which may be added to the polymer composition include, for example, calcium stearate, zinc stearate, stearic acid, or mixtures thereof.

With particular reference to medium and high 10 voltage cables, the polymer materials as defined hereinabove may be advantageously used to obtain an insulating layer. As stated above, these polymer mechanical good indeed show materials characteristics both at ambient temperature and 15 under hot conditions, and also show improved electrical properties. In particular they enable high operating temperature to be reached, comparable with or even exceeding that of cables with coverings consisting of crosslinked polymer base materials. 20

If a semiconductive layer has to be formed, a conductive filler, in particular carbon black, is generally dispersed within the polymer base material in a quantity such as to provide the material with semiconductive characteristics (i.e. such as to obtain a resistivity of less than 5 Ohm\*m at ambient temperature). This quantity is generally between 5 and 80 wt%, and preferably between 10 and 50 wt%, of the total weight of the mixture.

The use of the same polymer composition for both the insulating layer and the semiconductive layers is particularly advantageous in producing cables for medium or high voltage, in that it ensures excellent adhesion between adjacent layers and hence a good electrical behaviour, particularly at the interface between the insulating layer and the inner

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semiconductive layer, where the electrical field and hence the risk of partial discharges are higher.

The polymer composition of the present invention may be prepared by mixing together the thermoplastic polymer material, the dielectric liquid and any other additives possibly present by using methods known in the art. Mixing may be carried out for example by an internal mixer of the type with tangential rotors (Banbury) or with interpenetrating rotors, or, preferably, in a continuous mixer of Ko-Kneader (Buss) type, or of co- or counter-rotating double-screw type.

Alternatively, the dielectric liquid of the present invention may be added to the thermoplastic polymer material during the extrusion step by direct injection into the extruder cylinder as disclosed, for example, in International Patent Application W002/47092 in the name of the Applicant.

According to the present invention, the use of the aforedefined polymer composition in cable covering layers for medium or high voltage enables recyclable, flexible coverings to be obtained with excellent mechanical and electrical properties.

Greater compatibility has also been found between the dielectric liquid and the thermoplastic polymer material of the present invention than in the case of similar mixtures of the same polymer material with other dielectric liquids known in the art. This greater compatibility leads, inter alia, to less exudation of the dielectric liquid. Due to their high operating temperature and their low dielectric losses, the cables of the invention can carry, for the same voltage, a power at least equal to or even greater than that transportable by a traditional cable with XLPE covering.

For the purposes of the invention the term

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"medium voltage" generally means a voltage between 1 kV and 35 kV, whereas "high voltage" means voltages higher than 35 kV.

Although this description is mainly focused on production of cables for transporting distributing medium or high voltage energy, polymer composition of the invention may be used for covering electrical devices in general particular cables of different type, for example low voltage cables, telecommunications cables energy/telecommunications cables, or combined accessories used in electrical lines, such as terminals, joints or connectors.

Further characteristics will be apparent from the detailed description given hereinafter with reference to the accompanying drawing, in which:

- Figure 1 is a perspective view of an electric cable, particularly suitable for medium or high voltage, according to the invention.

20 In Figure 1, the cable (1) comprises a conductor (2), an inner layer with semiconductive properties intermediate layer with insulating (3), an properties (4), an outer layer with semiconductive properties (5), a metal screen (6), and an outer sheath (7). 25

The conductor (2) generally consists of metal wires, preferably of copper or aluminium, stranded together by conventional methods, or of a solid aluminium or copper rod. At least one covering layer selected from the insulating layer (4) semiconductive layers (3) and (5) comprises the composition of the invention as heretofore defined. Around the outer semiconductive layer (5) there is usually positioned a screen (6), generally of electrically conducting wires or strips wound helically. This screen is then covered by a sheath

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of a thermoplastic material such as, for example, non-crosslinked polyethylene (PE).

The cable can be also provided with a protective structure (not shown in Figure 1) the main purpose of which is to mechanically protect the cable against impacts or compressions. This protective structure may be, for example, a metal reinforcement or a layer of expanded polymer as described in WO 98/52197 in the name of the Applicant.

Figure 1 shows only one possible embodiment of a 10 Suitable invention. to the according cable modifications known in the art can be made to this embodiment, but without departing from the scope of the invention.

cable covering layer or layers 15 The thermoplastic material according to the present invention may be manufactured in accordance with example by extrusion. The known methods, for extrusion is advantageously carried out in a single pass, for example by the tandem method in which 20 individual extruders are arranged in series, or by co-extrusion with a multiple extrusion head.

The following examples illustrate the invention, but without limiting it.

#### 25 EXAMPLES 1-5

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#### Compositions preparation

The following components were used:

- a propylene heterophase copolymer with melting point 165°C, melting enthalpy 30 J/g, MFI 0.8 dg/min and flexural modulus 150 MPa (Adflex Q 200 F - commercial product of Basell);
- a propylene heterophase copolymer with melting point 142°C, melting enthalpy 25 J/g, MFI 0.6 dg/min and flexural modulus of 85 MPa (Hifax CA 10A - commercial product of Basell);
- Sunpar 2280 (commercial product of Sunoco):

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paraffinic oil with viscosity of 475 cSt at 40°C, pour point of -15°C and ratio of number of aromatic carbon atoms with respect to the total number of carbon atoms of 0.02, consisting of 69 %wt paraffinic carbon atoms, 29 wt% naphthenic carbon atoms, 2 wt% aromatic carbon atoms and 1.5 wt% polar compounds;

- Nyflex® 820 (commercial product of Nynas):
  naphthenic oil with viscosity of 110 cSt at
  40°C, pour point of -27°C and ratio of number of
  aromatic carbon atoms with respect to the total
  number of carbon atoms of 0.1, consisting of 10
  % the aromatic carbon atoms, 46 wt% naphthenic
  carbon atoms, 44 wt% paraffinic carbon atoms and
  0.2 wt% polar compounds;
- Nytex\* 840 (commercial product of Nynas):
  naphthenic oil with with viscosity of 370 cSt at
  40°C, pour point of -12°C and ratio of number of
  aromatic carbon atoms with respect to the total
  number of carbon atoms of 0.15, consisting of 15
  %wt aromatic carbon atoms, 34 wt% naphthenic
  carbon atoms, 51 wt% paraffinic carbon atoms and
  2.3 wt% polar compounds;

The polymer in granular form was preheated,

25 under agitation, at 80°C, over 15 min, in a
turbomixer. Subsequently, the dielectric liquid, 6%
by weight, was added to the preheated polymer. After
the addition, agitation was continued for 2 hours at
80°C until the liquid was completely absorbed in the
polymer granules.

After this first stage, the resultant material was kneaded in a laboratory double-screw Brabender Plasticorder PL2000 at a temperature of 180°C to complete homogenization. The resultant material left the double-screw mixer in the form of granules.

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#### Measurement of dielectric losses

Plates of 0.5 mm thickness were formed from the material obtained as disclosed above. The plates were moulded at 195°C with 15 min preheating.

plates obtained in this manner were subjected to dielectric loss measurement by measuring the tangent of the loss angle (tandelta) (according to ASTM standarrd D150) at. various temperatures and at various gradients (G). measurements at G = 10 kV/mm were effected under a pressure of 25 bar of nitrogen. The tandelta  $\times$  10<sup>-4</sup> (G = 2 kV/mm at 50 Hz) at 20°C was of between 3 and 50 and the tandelta  $\times$  10<sup>-4</sup> (G = 2 kV/mm at 50 Hz) at 90°C was of between 5 and 100.

#### 15 Measurement of flexural modulus

The flexural modulus was determined on plates 60 mm x 10 mm x 1.5 mm obtained as disclosed above in accordance with ASTM standard D790: the obtained results are given in Table 1.

Measurement of melting point  $(T_m)$  and 20 melting enthalpy (AH)

The melting point (Tm) and the melting enthalpy  $(\Delta H)$ were determined Differential by Scanning Calorimetry (DSC) analysis by using a Mettler Toledo 820 differential scanning calorimeter. temperature program below was applied to the sample to be analysed:

- cooling from room temperature to -100°C;
- heating from -100°C to 200°C at a rate of 30 10°C/min.;
  - isotherm for 5 minutes at 200°C;
  - cooling to -100°C at a rate of 2°C/min.;
  - isotherm for 10 minutes at -100°C;
  - heating to 200°C at a rate of 10°C/min.
- 35 The obtained results are given in Table 1.

23 TABLE 1

EXAMPLE	Flexural modulus (MPa)	Melting point (Tm) (°C)	Melting enthalpy (ΔH) (J/g)
1	37	162	40.2
2	35	163	40.9
3	30	160	41.1
4	60	139	30.7
5	60	140	32.0

Example 1: 94% by weight Adflex Q 200 F + 6% by weight Sunpar 2280;

Example 2: 94% by weight Adflex Q 200 F + 6% by 5 weight Nyflex 820;

Example 3: 94% by weight Adflex Q 200 F + 6% by weight Nytex 840;

Example 4: 94% by weight Hifax CA 10 A + 6% by weight Sunpar 2280;

Example 5: 94% by weight Hifax CA 10 A + 6% by weight Nytex 2280.

#### EXAMPLE 6

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#### Measurement of the saturation concentration

In order to determine the saturation concentration of the dielectric liquid in the thermoplastic materials, a plurality of plates were manufactured starting from the raw materials in pellets.

Two plates (200 mm  $\times$  200 mm  $\times$  0.5 mm) were 20 obtained by molding the raw material (Adflex Q 200 F) at 190°C. Five smaller Dumbell samples were

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obtained from each of the above plates and weighted  $(W_0)$ .

The Dumbell samples were then totally immersed at  $20\,^{\circ}\text{C}$ , into a dielectric liquid: Sunpar 2280 and Nyflex 820, respectively. The saturation concentration was measured by determining the weight change (in percentage) of the plates after different times. The Dumbell samples were removed from the dielectric liquid after 3, 6, 9, 12 and 15 days, and after having cleaned their surface with a dry and clean cloth, they were weighted (Wi).

The dielectric liquid absorption was determined by the following formula:

% of absorbed dielectric liquid =  $[(W_1 - W_0)/W_0] \times 100$ .

The saturation concentration is reached when  $W_i$  shows a variation lower than 1% with respect to the toatal weight increase which correspond to  $(W_i - W_0)$ .

The obtained results were the following:

- the saturation concentration of Sunpar® Q 200 F in the Adflex® Q 200 F is higher than 6% by weight;
- the saturation concentration of Nyflex® 820 in the Adflex® Q 200 F is higher than 12% by weight.

#### EXAMPLE 7

In order to verify the absence of two phases, 25 the absence of a continuos phase of thermoplastic material and of an additional phase incorporated therein of a dielectric liquid, samples liquid . as and of auch of the dielectric with the material additioned thermoplastic 30 dielectric liquid were subjected to the Modulated Differential Scanning Calorimetry (MDSC) analysis 2920 Modulated DSC Instrument TA a using differential scanning calorimeter.

35 10 mg of each sample were subjected to the following temperature program:

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- equilibrating at -145°C;
- modulating ±0.48°C every 60 seconds;
- keeping at -145°C for 5 minutes;
- heating to 200°C at a rate of 5°C/min;
- 5 keeping at 200°C for 2 minutes. The obtained results are given in Table 2.

#### TABLE 2

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EXAMPLE	MDSC ANALYSIS
Sunpar 2280	-0.59°C
Adflex Q 200 F + 6% Sunpar 2280	absent
Adflex Q 200 F + 20% Sunpar 2280	-0.59°C

The results in Table 2 show that:

- in the case the dielectric liquid as such, a peak at -0.59°C was present;
- dielectric liquid in the case the 15 thermoplastic material added the in quantity (6% by weight) not higher than its saturation concentration in said thermoplastic material, the peak at -0.59°C, characteristic of the dielectric liquid as such, was not present, 20 liquid showing that the dielectric microscopically homogeneously dispersed in the thermoplastic material;
- in the case the dielectric liquid is added to the thermoplastic material in a quantity (20% by 25 weight) higher than its saturation concentration said thermoplastic material, the peak at -0.59°C, characteristic of the dielectric liquid

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as such, was present, showing that the dielectric liquid was not microscopically homogeneously dispersed in the thermoplastic material.

## 5 EXAMPLES 8-9 (comparative)

## Compositions preparation

The following components were used:

- a propylene heterophase copolymer with melting point of 142°C, melting enthalpy 25 J/g, melting point 142°C, MFI 0.6 dg/min and flexural modulus of 85 MPa (Hifax CA 10A commercial product of Basell);
- Nytex® 800 (commercial product of Nynas):
  naphthenic oil with viscosity of 7.3 cst at
  40°C, pour point of -60°C and ratio of number of
  aromatic carbon atoms with respect to the total
  number of carbon atoms of 0.07, consisting of 7
  wt% aromatic carbon atoms, 53 wt% naphthenic
  carbon atoms, 40 wt% of paraffinic carbon atoms
  and 0.5 wt% polar compounds;
  - Indopol<sup>®</sup> L-100 (commercial product of BP Amoco): polybutene oil with viscosity of 210 cSt at 40°C, pour point of -30°C and 0.5 wt<sup>§</sup> polar compounds.
- 25 The polymer in granular form was preheated, under agitation, at 80°C, over 15 min, in a turbomixer. Subsequently, the dielectric liquid, 6% by weight, was added to the preheated polymer. After the addition agitation was continued for 2 hours at 80°C until the liquid was completely absorbed in the polymer granules.

After this first stage, the resultant material was kneaded in a laboratory double-screw Brabender Plasticorder PL2000 at a temperature of 150°C to complete homogenization. The resultant material left the double-screw mixer in the form of granules.

#### EXAMPLE 10

## Scanning Electron Microscopy (SEM)

Scanning Electron Microscopy (SEM) analysis was conducted as follows by utilizing the compositions 5 of Examples 1-5 (according to the present invention) and the compositions of Examples 8-9 (comparative). Compression molded tensile samples were notched with a razor blade and subsequently immersed in liquid nitrogen. Samples were then fractured in a compact tension mode. Freeze-fracture morphology of gold 10 coated samples was examined with a Hitachi 5-400 SEM operating at 10 KV. Digital image analysis was performed on a series of micrographs to determine the presence of a single-phase material or of a two-5000X the surfaces of the phases material. At 15 samples obtained from the compositions of Examples (according to the present invention) were homogeneous and devoid of cavity showing that the single phase material. material is at 5000X, the surfaces of the samples contrary, 20 obtained from the compositions of Example 6 and 7 (comparative), were not homogeneous and presented a lot of cavity showing that the material is a two phase material. Moreover, the samples obtained from Examples 8-9, showed exudation of the dielectric 25 liquid at room temperature.

#### EXAMPLE 11

#### Cable production

The compositions of the insulating layer and of the semiconductive layers are described in Table 3 below.

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TABLE 3

	_	ording to resent ntion	Comparison cable		
	Inner and outer semicond. layers	Insulation layer	Inner and outer semicond. layers	Insulation layer	
	(육)	(七)	· (융)	(육)	
	by weight	by weight	by weight	by weight	
Adflex®	60.4	93.4	66.4	99.4	
Ensaco <sup>®</sup> 250 G	33.	-	33	_	
Sunpar <sup>®</sup> 2280	6	6	-	-	
Irganox°	0.4	0.4	0,4	0.4	
Irganox <sup>®</sup>	0.2	0.2	0.2	0.2	

Ensaco 250 G: carbon black with specific surface of 65 m2/g (commercial product of MMM Carbon);

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Irganox® PS 802 (antioxidant): distearyl
 thiodipropionate (commercial product of Ciba
 Specialty Chemicals);

Irganox 1010 (antioxidant): pentaerithrityl-

tetrakis-(3-(3,5-di-t-butyl-4-hydroxy-phenyl)propionate (commercial product of Ciba Specialty
Chemicals).

The process used for manufacturing the cable was the following.

The Adflex Q 200 F was fed directly into the 10 extruder hopper. Subsequently, the Sunpar 2280 previously mixed with the antioxidants, was injected at high pressure into the extruder. An extruder having a diameter of 80 mm and an L/D ratio of 25 15 injection was made during the used. The extrusion at about 20 D from the beginning of the extrduder screw by means of three injections point on the same cross-section at 120° from each other. The dielectric liquid was injected at a temperature 20 of 70°C and a pressure of 250 bar.

The cable leaving the extrusion head was cooled to ambient temperature by passing it through cold water.

The finished cable consisted of an aluminum conductor (cross-section 150 mm<sup>2</sup>), an inner semiconductive layer of about 0.5 mm in thickness, an insulating layer of about 4.5 mm in thickness and finally an outer semiconductive layer of about 0.5 mm in thickness.

30 Under similar conditions, by using the materials indicated in Table 2, a comparison cable was produced without adding the dielectric liquid.

Dielectric strength

Three pieces (each being 20 metres in length) of 35 the two cables produced as described above were subjected to dielectric strength measurement using

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alternating current at ambient temperature. Starting from 100 kV the gradient applied to the cables was increased by 10 kV every 10 minutes until the cables broke down. The break down gradient considered is that on the conductor.

Table 4 summarizes the results of the electrical tests: the data represent the average value obtained from three different measurements.

#### TABLE 4

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	Cable according to the present invention	Comparison cable
	(kV/mm)	(kV/nm)
AC break down	59	29

## EXAMPLE 12 (comparison)

#### Cable production

The compositions of the insulation layer is described in Table 5 below.

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#### TABLE 5

	COMPOSITION OF THE INSULATION LAYER
	(%) by weight
Adflex <sup>®</sup> Q 200 F	79.4
Sunpar 2280	20
Irganox® PS 802	0.4
Irganox 1010	0.2

The process used for manufacturing the cable was the following.

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The Adflex Q 200 F was fed directly into the extruder hopper. An extruder having a diameter of 80 mm and an L/D ratio of 25 was used. Subsequently, an attempt was made to inject the Sunpar 2280 previously mixed with the antioxidants into the extruder. The injection was impossible to be carried out since the dielectric liquid exit the extruder die. Consequently, the production of a finished cable was impossible to be carried out.

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#### CLAIMS

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- least 1. Cable comprising at one electrical conductor and at least one extruded covering. layer based on a thermoplastic polymer material in admixture with a dielectric liquid, wherein:
  - said thermoplastic polymer material selected from:
    - (a) at least one propylene homopolymer or at least one copolymer of propylene with at least one olefin comonomer selected from ethylene and an α-olefin other propylene, said homopolymer or copolymer having a melting point greater than or equal to 130°C and a melting enthalpy of from 20 J/g to 100 J/g;
    - (b) a mechanical mixture comprising at least one propylene homopolymer or copolymer (a) and (c) at least one elastomeric copolymer of ethylene with at least one aliphatic \alpha-olefin, and optionally a polyene;
  - concentration by weight of said the in said thermoplastic dielectric liquid polymer material is less or equal to the saturation concentration of said dielectric thermoplastic liquid in said material;
  - said dielectric liquid has the following characteristics:
    - an amount of polar compounds lower than or equal to 2.5% by weight with respect to the total weight of the dielectric liquid:
  - a melting point or a pour point lower. than 80°C:

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- a ratio of number of aromatic carbon atoms with respect to the total number of carbon atoms lower than 0.6, when the dielectric liquid is aromatic.
- 5 2. Cable according to claim 1, wherein the propylene homopolymer or copolymer (a) has a melting point of from 140°C to 170°C.
  - 3. Cable according to claim 1 or 2, wherein the propylene homopolymer or copolymer (a) has a melting enthalpy of from 30 J/g to 85 J/g.
  - 4. Cable according to any one of the preceding claims, wherein the propylene homopolymer or copolymer (a) has a flexural modulus, measured according to ASTM standard D790, at room temperature, of from 30 MPa to 1400 MPa.
  - 5. Cable according to claim 4, wherein the propylene homopolymer or copolymer (a) has a flexural modulus, measured according to ASTM standard D790, at room temperature, of from 60 MPa to 1000 MPa.
  - 6. Cable according to any one of the preceding claims, wherein the propylene homopolymer or copolymer (a) has a melt flow index (MFI), measured at 230°C with a load of 21.6 N according to ASTM standard D1238/L, of from 0.05 dg/min to 10.0 dg/min.
  - 7. Cable according to claim 6, wherein the propylene homopolymer or copolymer (a) has a melt flow index (MFI), measured at 230°C with a load of 21.6 N according to ASTM standard D1238/L, of from 0.4 dg/min to 5.0 dg/min.
  - 8. Cable according to any one of the preceding claims, wherein in the propylene copolymer (a) the olefin comonomer is present in a quantity of less than or equal to 15 mol%.
  - 9. Cable according to claim 8, wherein in the

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propylene copolymer (a) the olefin comonomer is present in a quantity of less than or equal to 10 mol%.

- 10. Cable according to any one of the preceding claims, wherein in the propylene copolymer (a) the olefin comonomer is ethylene or an α-olefin of formula CH<sub>2</sub>=CH-R, where R is a linear or branched C<sub>2</sub>-C<sub>10</sub> alkyl.
- 11. Cable according to claim 10, wherein the αolefin is selected from: 1-butene, 1-pentene, 4methyl-1-pentene, 1-hexene, 1-octene, 1-decene, 1-dodecene, or mixtures thereof.
  - 12. Cable according to any one of the preceding claims, wherein the propylene homopolymer or copolymer (a) is selected from:
    - (a<sub>1</sub>) a propylene homopolymer or a copolymer of propylene with at least one olefin comonomer selected from ethylene and an αolefin other than propylene, having a flexural modulus generally of from 30 MPa to 900 MPa;
    - (a<sub>2</sub>) a heterophase copolymer comprising a thermoplastic phase based on propylene and an elastomeric phase based on ethylene copolymerized with an α-olefin.
  - 13. Cable according to claim 12, wherein the propylene homopolymer or copolymer of class (a<sub>1</sub>) has a melting point of from 140°C to 170°C.
- 14. Cable according to claim 12 or 13, wherein the propylene homopolymer or copolymer of class (a<sub>1</sub>) has a melting enthalpy of from 30 J/g to 80 J/g.
- 15. Cable according to any one of claims 12 to 14, wherein the propylene homopolymer or copolymer of class (a<sub>1</sub>) has a fraction soluble in boiling diethyl ether in an amount of less than or equal to 12 wt%, having a melting enthalpy of less

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than or equal to 4 J/g.

- 16. Cable according to any one of claims 12 to 15, wherein the propylene homopolymer or copolymer of class (a1) has a fraction soluble in boiling n-heptane in an amount of from 15 wt% to 60 wt%, having a melting enthalpy of from 10 J/g to 40 J/g.
- 17. Cable according to any one of claims 12 to 16, wherein the propylene homopolymer or copolymer 10 of class (a1) has a fraction insoluble in boiling n-heptane in an amount of from 40 wt% to 85 wt%, having a melting enthalpy of greater than or equal to 45 J/g.
- 18. Cable according to claim 12, wherein the  $\alpha$ -15 olefin included in the elastomeric phase of a heterophase copolymer of class (a2) is propylene.
  - 19. Cable according to claim 12, wherein heterophase copolymer οf class  $(a_2)$ is heterophase copolymer in which the elastomeric phase consists of an elastomeric copolymer of ethylene and propylene comprising from 15 wt% to 50 wt% of ethylene and from 50 wt% to 85 wt% of propylene with respect to the weight of the elastomeric phase.
- 25 20. Cable according to any one of the preceding claims, wherein the elastomeric copolymer of ethylene (c) has a melting enthalpy of less than 30 J/g.
- 21. Cable according to any one of the preceding 30 claims, wherein the quantity of the elastomeric copolymer (c) is less than 70% with respect to the total weight of the thermoplastic base material.
- 22. Cable according to any one of the preceding 35 claims, wherein in the elastomeric copolymer of ethylene (c), the term "aliphatic  $\alpha$ -olefin" is

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- an olefin of formula  $CH_2=CH-R$ , in which R represents a linear or branched alkyl group containing from 1 to 12 carbon atoms.
- 23. Cable according to claim 22, wherein the aliphatic α-olefin is selected from propylene, 1-butene, isobutylene, 1-pentene, 4-methyl-1-pentene, 1-hexene, 1-octene, 1-dodecene, or mixtures thereof.
- 24. Cable according to claim 23, wherein the aliphatic  $\alpha$ -olefin is selected from propylene, 1-hexene, 1-octene.
  - 25. Cable according to any one of the preceding claims, wherein in the elastomeric copolymer of ethylene (c), the term "polyene" is a conjugated or non-conjugated diene, triene or tetraene.
  - 26. Cable according to claim 25, wherein the polyene is a diene.
  - 27. Cable according to any one of the preceding claims, wherein the elastomeric copolymer of ethylene (c) is selected from:
    - (c<sub>1</sub>) copolymers having the following monomer composition: 35 mol\*-90 mol\* of ethylene; 10 mol\*-65 mol\* of an aliphatic  $\alpha$ -olefin; 0 mol\*-10 mol\* of a polyene.
  - (c<sub>2</sub>) copolymers having the following monomer composition: 75 mol<sup>3</sup>-97 mol<sup>3</sup> of ethylene; 3 mol<sup>3</sup>-25 mol<sup>3</sup> of an aliphatic α-olefin; 0 mol<sup>3</sup>-5 mol<sup>3</sup> of a polyene.
- 28. Cable according to any one of the preceding claims, wherein the dielectric liquid has an amount of polar compounds of between 0.1 and 2.3.
- 29. Cable according to any one of the preceding claims, wherein the dielectric liquid has a melting point or a pour point of between -130°C and +80°C.

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- 30. Cable according to any one of the preceding claims, wherein the dielectric liquid has a ratio of number of aromatic carbon atoms with respect to the total number of carbon atoms of between 0.01 and 0.4.
- 31. Cable according to any one of the preceding claims, wherein the dielectric liquid has a dielectric constant, at 25°C, of less than or equal to 3.5 (measured in accordance with IEC 247).
- 32. Cable according to any one of the preceding claims, wherein the dielectric liquid has a viscosity, at 40°C, of between 10 cSt and 800 cSt (measured according to ASTM standard D445).
- 15 33. Cable according to claim 32, wherein the dielectric liquid has a viscosity, at 40°C, of between 20 cSt and 500 cSt (measured according to ASTM standard D445).
- 34. Cable according to any one of the preceding claims, wherein the dielectric liquid is selected from: mineral oils such as naphthenic oils, aromatic oils, paraffinic oils, polyaromatic oils, said mineral oils optionally containing at least one heteroatom selected from
- oxygen, nitrogen or sulphur; liquid paraffins; vegetable oils such as soybean oil, linseed oil, castor oil; oligomeric aromatic polyolefins; paraffinic waxes such as polyethylene waxes,
- polypropylene waxes; synthetic oils such such benzeness as silicone oils, alkyl 30 di (octylbenzyl) toluene, dodecylbenzene, of as tetraesters aliphatic esters such esters of sebacic pentaerythritol, phthalic acid esters, olefin oligomers such as
- optionally hydrogenated polybutenes or polyisobutenes; or mixtures thereof.

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- 35. Cable according to claim 34, wherein the dielectric liquid is selected from paraffinic oils, naphthenic oils.
- 36. Cable according to any one of the preceding claims, wherein the weight ratio of dielectric liquid to thermoplastic polymer material is between 1:99 and 25:75.
- 37. Cable according to claim 36, wherein the weight ratio of dielectric liquid to thermoplastic polymer material is between 2:98 and 20:80.
- 38. Cable according to claim 37, wherein the weight ratio of dielectric liquid to thermoplastic polymer material is between 3:97 and 10:90.
- 39. Cable according to any one of the preceding claims, wherein the thermoplastic polymer material is selected from propylene homopolymers or copolymers comprising at least 40 wt% of amorphous phase, with respect to the total polymer weight.
- 20 40. Cable according to any one of the preceding claims, wherein the extruded covering layer based on said thermoplastic polymer material in admixture with said dielectric liquid is an electrically insulating layer.
- 25 41. Cable according to any one of the preceding claims, wherein the extruded covering layer based on said thermoplastic polymer material in admixture with said dielectric liquid is a semiconductive layer.
- 30 42. Polymer composition comprising a thermoplastic polymer material in admixture with a dielectric liquid, wherein:
  - said thermoplastic polymer material is selected from:
- 35 (a) at least one propylene homopolymer or atleast one copolymer of propylene with at

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least one olefin comonomer selected from and an α-olefin other than propylene, said homopolymer or copolymer having a melting point greater than or equal to 130°C and a melting enthalpy of from 20 J/g to 100 J/g;

- (b) a mechanical mixture comprising at least one propylene homopolymer or copolymer and (c) at least one elastomeric (a) copolymer of ethylene with at least one aliphatic  $\alpha$ -olefin, and optionally a polyene;
- concentration by weight of. said the dielectric liquid in said thermoplastic polymer material is less or equal to the saturation concentration of said dielectric thermoplastic liquid said material;
- said dielectric liquid has the following characteristics:
  - an amount of polar compounds lower than or equal to 2.5% by weight with respect to the total weight of the dielectric liquid;
- a melting point or a pour point lower 25 than 80°C;
  - a ratio of number of aromatic carbon atoms with respect to the total number of carbon atoms lower than 0.6, when the dielectric liquid is aromatic.
  - 43. Polymer composition according to claim 42, wherein the thermoplastic polymer material is defined according to any one of claims 2 to 27.
- 44. Polymer composition according to claim 42 or 43, wherein the dielectric liquid 35 is according to any one of claims 28 to 38,

- 45. Use of the polymer composition defined according to any one of claim 42 to 44, as the polymer base material for preparing a cable covering layer with electrical insulation properties.
- 5 45. Use of the polymer composition defined according to any one of claim 42 to 44, as the polymer base material for preparing a cable covering layer with semiconductive properties.

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#### ABSTRACT

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Cable comprising at least one electrical conductor and at least one extruded covering layer based on a thermoplastic polymer material in admixture with a dielectric liquid, wherein:

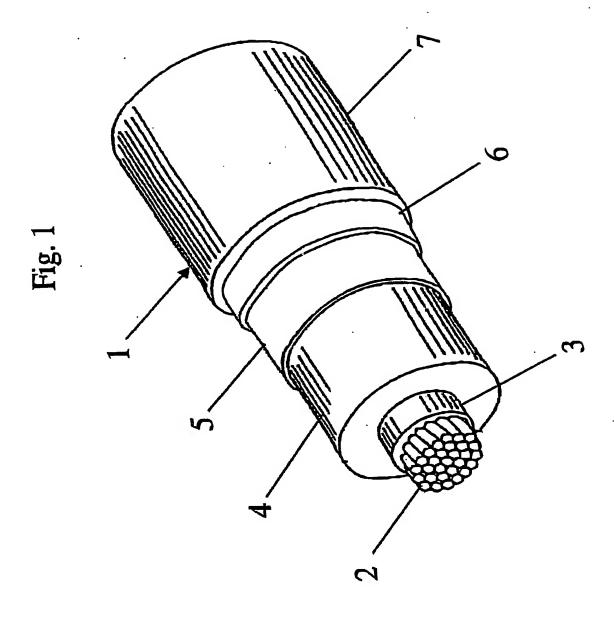
- said thermoplastic polymer material is selected
  from:
  - (a) at least one propylene homopolymer or at least one copolymer of propylene with one olefin comonomer selected from least α-olefin other than ethylene and an propylene, said homopolymer or copolymer having a melting point greater than or equal to 130°C and a melting enthalpy of from 20 J/g to 100 J/g;
  - (b) a mechanical mixture comprising at least one propylene homopolymer or copolymer (a) and (c) at least one elastomeric copolymer of ethylene with at least one aliphatic  $\alpha$ -olefin, and optionally a polyene;
- the concentration by weight of said dielectric liquid in said thermoplastic polymer material is less or equal to the saturation concentration of said dielectric liquid in said thermoplastic polymer material;
- said dielectric liquid has the following characteristics;
- an amount of polar compounds lower than or equal to 2.5% by weight with respect to the total weight of the dielectric liquid;
  - a melting point or a pour point lower than 80°C;
- a ratio of number of aromatic carbon atoms
  35 with respect to the total number of carbon

atoms lower than 0.6, when the dielectric liquid is aromatic.

The cable of the invention possesses good mechanical and electrical properties, including high dielectric strength, in particular enabling it to be used at high operating temperature.

Fig. 1.

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